

Resonant grazing bifurcations in simple impacting systems

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Impact Oscillators



Many engineering systems involve vibrations and impacts.



Figure: Examples of simple impacting systems: (a) a bell, (b) a gear assembly, (c) an impact print hammer. Picture taken from di Bernardo *et al.* (2008)

Mechanical devices are often engineered with loose-fitting joints to accommodate thermal expansion, and the dynamics of this often lead to impacts in the joint.

Literature Survey (the 80's & 90's)





Figure 1. The physical system.

(a) S.W. Shaw et al., 1983.





Literature Survey (the 2000's)





Fig. 1. The geometry of a rectangular plate under transversal forcing.

(a) J. Qiu and Z.C. Feng, 2000.



FIG. 1. Schematic diagram of the experimental rig [3].

(d) S. Banerjee et al., 2009.



Figure 2. The physical system studied in this paper. The mass se of the oscillator can collide with a yielding wild. We assume that the mankets will is statubed with frictionless springs to the fixed work? The solutions of the wall is determined by the stiffness of the second spring. We use merganized units with n = -1, the wall position at rest at n = 0, and the rest position of the colliding mass in n = -1.

(b) J. Molenaar *et al.*, 2001.



(e) J. Ing et al., 2011.

20 If T.Fuence, L.N. Vaga, and A.R. Chapterget The result of the second secon

(c) P. T. Piiroinen *et al.*, 2004.



Fig. 2, (c) The Scotch pole finding mechanism. (b) the data acquisition camera and its mounting position relative to the pendulum spin



Fig. 1. (c) The double produlum sprices in its spright position, (b) produlum sprices attached is the duales; (c) sechastion allowing to plane and plane till, (c) close-up of small possiblem ME

(f) T. Witelski et al., 2014.

An experimental example





Figure: Bifurcation diagram obtained from the paper by Pavlovskaia et al., 2010.

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Why does a stable period-two solution appear so close to grazing?

A linear oscillator with hard impacts





Figure: Equations: $\ddot{x} + b\dot{x} + x + 1 = F\cos(\omega t)$ and $\dot{x} \mapsto -r\dot{x}$ whenever x = 0. The oscillator is under-damped (0 < b < 2). Let F be the primary bifurcation parameter and ω be the second.

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- ▶ If the block hits the wall with zero velocity, this is a *grazing* impact.
- A grazing bifurcation occurs when the limit cycle has a grazing impact.

Typical phase portrait and bifurcation diagram





Grazing occurs at $F = F_{\text{graz}}(\omega)$, where $F_{\text{graz}}(\omega) = \sqrt{(1-\omega^2)^2 + b^2 \omega^2}$.

Two-parameter bifurcation diagram





Figure: See Ivanov (1993), and Nordmark (2001).

Poincaré map





• Let $y(t) = \dot{x}(t)$ and $z = (t - t_{ref}) \mod \frac{2\pi}{\omega}$.

Poincaré map





Let y(t) = x(t) and z = (t − t_{ref}) mod ^{2π}/_ω.
Use y = 0 as the Poincaré section. The map: (x', z') = P(x, z) where P = P_{global} ∘ P_{disc}.

Poincaré map



For a parameter $\mu \in \mathbb{R}$,

$$P_{\text{global}}(x,z;\mu) = A \begin{bmatrix} x \\ z \end{bmatrix} + q\mu + \mathcal{O}((|x|+|z|+|\mu|)^2),$$

where $A = \mathrm{D}P_{\mathrm{global}}(0,0;0)$, and $q = \frac{\partial P_{\mathrm{global}}}{\partial \mu}(0,0;0)$.

The discontinuity map by Nordmark is given by

$$P_{\rm disc}(x,z;\mu) = \begin{cases} \begin{bmatrix} x\\z \end{bmatrix}, & x \le 0, \\\\ \begin{bmatrix} r^2x + \tilde{O}(3)\\ z - \frac{\sqrt{2}}{\omega}(1+r)\sqrt{x} + \tilde{O}(2) \end{bmatrix}, & x > 0. \end{cases}$$



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- ▶ We continue zeros of the function $G = P_{\text{global}}^p \circ P_{\text{disc},R} I$.



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- ▶ The function V maps the Velocity Into Variation In Displacement.
- This function is smooth in a neighborhood of $(y_1, z_1) = (0, 0)$.

One-parameter bifurcation diagrams





Resonance



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Here

$$\tau = 2e^{-\frac{\pi b}{\omega}}\cos\left(\frac{2\pi\xi}{\omega}\right), \qquad \delta = e^{-\frac{2\pi b}{\omega}}$$



Figure: Division of the (τ, δ) plane.





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For the linear impact oscillator,

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i) for
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, we have $a_{1,2} = 0$ if and only if $\frac{\xi}{\omega^*} = \frac{n}{2}$, for some $n \in \mathbb{Z}$;
ii) for $p \ge 2$, we have $\tau = 2\sqrt{\delta} \cos\left(\frac{\pi}{p}\right)$ if and only if $\frac{\xi}{\omega^*} = n \pm \frac{1}{2p}$, for some $n \in \mathbb{Z}$

Asymptotics (p = 1)



Let $\eta = \omega - \omega^*$. For p = 1 let

$$c_{\pm,1} = \mp \left(1 + \phi^2 \delta^p\right) + a_{11}\phi^2 + a_{22} + \frac{\alpha^2 \ell}{(1 - a_{22})\gamma}.$$

Then

$$g_{\pm,1}(\eta) = \frac{\alpha^2 \left(\frac{da_{12}}{d\eta}\right)^2}{\beta \gamma c_{\pm,1}} \, \eta^2 + \mathcal{O}\left(\eta^3\right).$$

Asymptotics $(p \ge 2)$



Let

$$c_{\pm,p} = \mp \left(1 + \phi^2 \delta^p\right) - \sqrt{\delta^p} \left(1 + \phi^2\right) + \frac{\alpha^2 \ell}{\left(1 + \sqrt{\delta^p}\right) \gamma}.$$

Then

$$g_{+,p}(\eta) = \frac{\alpha^2 a_{12}^2 p^2 \delta^{p-2} (\delta - \tau + 1) (\kappa')^2}{8 \sin^4 \left(\frac{\pi}{p}\right) \left(1 + \sqrt{\delta^p}\right)^2 \beta \gamma c_{+,p}} \eta^2 + \mathcal{O}\left(\eta^3\right),$$

$$g_{-,p}(\eta) = \frac{\alpha^2 a_{12}^2 p^2 \delta^{p-2} (\delta - \tau + 1) (\kappa')^2 (1 - \frac{c_{+,p}}{2c_{-,p}})}{4 \sin^4 \left(\frac{\pi}{p}\right) \left(1 + \sqrt{\delta^p}\right)^2 \beta \gamma c_{-,p}} \eta^2 + \mathcal{O}\left(\eta^3\right).$$

Two-parameter bifurcation diagram with asymptotics





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- We have come up with a way of circumventing the issue of numerical algorithms falling off the side of square-root near grazing by using the VIVID function.
- We have also theoretically come up with matching asymptotics, unfolding the codimension-two points.
- ▶ Future: More complete bifurcation diagram, other bifurcation curves.

The End



Thank you! Questions?